

ANGLED PHYSICAL CONTACT FERRULE AND ASSOCIATED METHOD AND APPARATUS FOR FABRICATING SAME

FIELD OF THE INVENTION

5 The present invention relates generally to ferrules for mounting upon the end portions of optical fibers and, more particularly, to angled physical contact (APC) ferrules and associated methods and apparatus for fabricating APC ferrules.

BACKGROUND OF THE INVENTION

10 A variety of ferrules have been developed to facilitate the interconnection of optical fibers, with other optical fibers, optical devices or the like. For example, a number of standard ferrules, such as SC, FC, and ST ferrules, have been designed. Regardless of their type, ferrules typically define one or more longitudinal extending bores for receiving end portions of respective optical fibers.

15 One common type of ferrule is an APC ferrule that is designed to make physical contact with another APC ferrule during the process of interconnecting a pair of optical fibers. Notably, the front face of an APC ferrule is disposed at a nonorthogonal angle, i.e., at other than 90°, relative to the longitudinal axis defined by the ferrule. For example, the front face of an APC ferrule is commonly disposed at an angle of
20 approximately 8° relative to a plane that extends perpendicular to the longitudinal axis defined by the ferrule. In order to interconnect a pair of APC ferrules, the ferrules are therefore positioned such that the angled front faces are complimentary to one another, that is, the forwardmost portion of the front face of one ferrule is preferably aligned with the rearwardmost portion of the front face of the other ferrule and vice versa. In order to
25 facilitate the alignment of the ferrules in this complimentary fashion, the ferrules typically include a key that is disposed in a predetermined relationship to the front face of

the ferrule. Thus, a connector sleeve or the like can be utilized to engage the keys of a pair of APC ferrules to insure that the ferrules are mated in a complementary fashion.

The angled front face of an APC ferrule advantageously reduces undesirable reflections of optical signals at the interface between a pair of optical fibers, thereby decreasing optical power losses and correspondingly increasing optical power transmission. In addition to forming the ferrule to have a front face that is disposed at a predetermined angle relative to the longitudinal axis defined by the ferrule, the front face of some APC ferrules has a spherical shape. In this regard, if an APC ferrule is constructed such that the apex of the spherical surface substantially coincides with the bore defined by the ferrule, physical contact between the end portions of the respective optical fibers is facilitated, thereby enhancing optical transmission between the optical fibers. Unfortunately, it is relatively difficult to shape the spherical surface of an APC ferrule such that the apex of the spherical surface coincides with the bore defined by the ferrule. Instead, APC ferrules having a spherical front face generally have an apex offset that is defined as the distance by which the apex of the spherical surface is offset from the bore defined by the ferrule. While some apex offset can be tolerated while still maintaining optical transmission between the respective optical fibers, signal transmission can be adversely impacted if the apex offset becomes too large, such as greater than 50 microns. The degree of apex offset that can be tolerated is dependent upon several factors including whether the optical fibers are single mode or multimode, as well as the radius of curvature of the spherical surface. In this regard, greater apex offsets are typically acceptable for spherical surfaces having larger radii of curvature than for spherical surfaces having smaller radii of curvature.

Conventional APC ferrules that are to include a spherical front face typically require that the amount of material that is removed from the front face of the ferrule to define the spherical surface be precisely controlled so as to form the spherical surface in such a manner that the apex of the spherical surface coincides with the bore defined by the ferrule. In this regard, the removal of either too much or too little material during the process of grinding the front face of an APC ferrule into a spherical shape would typically result in the apex of the spherical surface being offset from the bore defined by the ferrule. In an attempt to minimize the apex effect, at least some of the prior

techniques for grinding the front face of an APC ferrule to define the spherical surface are relatively complex, thereby decreasing the efficiency and increasing the cost at which APC ferrules can be fabricated.

One exemplary APC ferrule is described by U.S. Patent No. 5,351,327 along with
5 several techniques for fabricating the APC ferrule. As described, the APC ferrule has a spherically shaped front face with an apex offset of no more than 50 microns and, more typically, no more than 10 microns. While several different fabrication techniques are described, most of the techniques require that the front face of the ferrule be formed into a temporary surface that is then repolished to form the desired spherical surface. The
10 temporary surface can be either flat or spherical and is typically angled or inclined relative to a plane perpendicular to the longitudinal axis defined by the ferrule. Unfortunately, the repolishing of the front face and the other finishing operations disadvantageously consume polishing consumables and reduce the efficiency with which the ferrules can be fabricated.

15 In addition, U.S. Patent No. 5,148,660 describes an APC ferrule having a spherical front surface that is angled relative to a plane perpendicular to the longitudinal axis defined by the ferrule. The APC ferrule described by U.S. Patent No. 5,140,660 includes a cylindrical tip or pedestal that extends forwardly from the main portion of the ferrule body and that has a smaller diameter than the main portion of the ferrule body. As
20 such, the cylindrical tip may damage surfaces that come into contact with the front face of the ferrule, such as by tearing polishing film or cleaning clothes.

While a number of APC ferrules have therefore been proposed that include spherical front faces, each of these conventional APC ferrules is subject to some shortcomings. For example, the process of grinding the front face of the ferrule may
25 have to be closely monitored since the removal of too much or too little material may disadvantageously increase the apex offset. In addition, some APC ferrules may require extensive polishing or other finishing operations such that the front face is sufficiently smooth, thereby increasing the fabrication costs and the resulting cost of the APC ferrules. Thus, with increasing emphasis being placed upon lowering the cost of ferrules
30 and reducing the permissible tolerances of the ferrules, an improved APC ferrule is desired that offers a reduced apex offset and that can be fabricated in a relatively simple

fashion, thereby reducing fabrication costs and the cost of the resulting APC ferrules relative to conventional fabrication techniques.

SUMMARY OF THE INVENTION

5 A ferrule is therefore provided that can be fabricated in a repeatable and an efficient manner so as to have a relatively small apex offset. In this regard, a method and apparatus for fabricating a ferrule are also provided that grind a portion of the front face of the ferrule into a hemispherical shape with a relatively small apex offset regardless of the amount of material that is removed from the front face of the ferrule. Since the apex
10 offset is not dependent upon the amount of material removed from the front face of the ferrule to define the hemispherical surface, the method and apparatus for fabricating the ferrule can be performed in a repeatable manner with a minimum number of finishing steps being required after the grinding process to complete the fabrication of the ferrule.

According to one advantageous aspect of the present invention, a ferrule is
15 provided that includes a ferrule body extending lengthwise between opposed front and rear faces and defining a longitudinal axis. The ferrule body also defines a lengthwise extending bore capable of receiving an end portion of an optical fiber. According to the present invention, the front face of the ferrule body includes a plateau defining a plane that extends perpendicular to the longitudinal axis and a hemispherical portion through
20 which the bore opens. Typically, the hemispherical portion is rearward of the plateau such that the plateau defines the forwardmost portion of the ferrule body.

The hemispherical portion of the front face of the ferrule body is preferably angled relative to the plateau and to the plane perpendicular to the longitudinal axis defined by the plateau. In this regard, a plane tangent to the hemispherical portion at a
25 point coincident with the longitudinal axis is disposed at an offset angle, typically between 8° and 12°, relative to the plane perpendicular to the longitudinal axis such that the resulting ferrule is an APC ferrule. The plateau is generally smaller than the hemispherical portion with the plateau typically extending across less than 50% of the front face of the ferrule body, and the hemispherical portion extending across more than
30 50% of the front face of the ferrule body. The plateau is also typically disposed proximate a side surface of the ferrule body and, in instances in which a portion of the

ferrule body proximate the front face is chamfered, the plateau is preferably disposed proximate the chamfer.

By constructing the ferrule to have a front face that includes a plateau and a hemispherical portion, the ferrule of the present invention provides an angled front face for minimizing reflections and for facilitating optical coupling with the optical fiber upon which the ferrule is mounted. In addition, the ferrule of the present invention can be readily fabricated such that the apex offset that is both repeatable and relatively small.

According to another aspect of the present invention, a method and apparatus for fabricating a ferrule, such as an APC ferrule, are provided. In this regard, the ferrule is initially secured within a mounting fixture, such as a collet, such that the front face of the ferrule is exposed. At this initial stage of the fabrication process, the front face of the ferrule is typically perpendicular to the longitudinal axis defined by the ferrule. A grinder is also provided that includes a spindle adapted for rotation about a spindle axis that is offset by a predetermined angle, such as between 8° and 12° , from a plane perpendicular to the longitudinal axis. The grinder also includes a grinding wheel mounted upon the spindle for rotation therewith about the spindle axis. To impact the spherical surface, the grinding wheel has an arcuate grinding surface that generally defines a radius of curvature of between 5 mm and 12 mm. The grinder is also adapted to rotate both the spindle and the grinding wheel about an offset axis that is orthogonal to the spindle axis and is coplanar with both the spindle axis and the longitudinal axis defined by the ferrule. Typically, the grinder rotates the spindle and the grinding wheel at a faster rate about the spindle axis than about the offset axis.

At least one of the grinding wheel and the ferrule is then advanced toward the other by means of a translation device such as a translation stage. In particular, the translation device advances at least one of the grinder and the mounting fixture toward the other along a motion axis that extends parallel to the longitudinal axis and that is coplanar with the spindle axis, the offset axis, and the longitudinal axis. During this advancement, the grinding wheel is rotated about both the spindle axis and the offset axis in order to engage and grind a portion of the front face of the ferrule into a hemispherical shape. Typically, the advancement of at least one of the grinder and the mounting fixture is halted prior to grinding all of the front face of the ferrule into a hemispherical shape

such that a portion of the front face of the ferrule remains as a plateau that extends substantially perpendicular to the longitudinal axis defined by the ferrule.

While either or both of the grinder and the mounting fixture can be advanced toward the other, a translation stage typically advances the grinder toward the ferrule
5 along the motion axis, while the mounting fixture remains fixed in position. In order to insure that the proper portion of the front face of the ferrule is ground into a hemispherical shape, the position of at least one of the ferrule and the grinder is adjusted relative to the other before commencing grinding. In this regard, the apparatus can include a plurality of adjustment stages for adjusting the position of the mounting fixture
10 in respective planes relative to the grinder.

By fabricating the ferrule according to the method and apparatus of the present invention, a ferrule having an at least partially angled front face and a relatively small apex offset, such as 50 microns or less, can be fabricated in a repeatable and an efficient manner. In this regard, since the front face of the ferrule has both a plateau and a
15 hemispherical portion, the apex offset is not dependent upon the amount of material removed from the front face during the process of grinding the hemispherical surface. As such, ferrules can be repeatedly fabricated that have approximately the same relatively small apex offset. In addition, the method and apparatus for fabricating the ferrule of the present invention also minimizes finishing steps that would otherwise have to be taken in
20 order to complete the fabrication of the ferrule, such as by minimizing the subsequent polishing of the front face of the ferrule since the grinding procedure also produces a relatively hemispherical surface. Thus, the efficiency of the fabrication process is increased and the costs of fabrication are potentially decreased.

25 BRIEF DESCRIPTION OF THE DRAWINGS

Figure 1 is a plan view of the front face of the ferrule according to one embodiment of the present invention.

Figure 2 is a cross-sectional view of the ferrule of Figure 1 taken along line 2-2.

Figure 3 is a schematic representation of the front face of a ferrule according to
30 one embodiment of the present invention illustrating the plateau and the hemispherical portion in more detail.

Figure 4 depicts an apparatus for fabricating a ferrule according to one embodiment to the present invention.

Figure 5 is a cross-sectional view of a ferrule and a ferrule holder for holding the ferrule during the grinding process.

5 Figure 6 is a schematic representation of at least a portion of an apparatus for fabricating a ferrule according to one embodiment of the present invention that illustrates the spindle and the grinding wheel in more detail.

DETAILED DESCRIPTION OF THE INVENTION

10 The present invention now will be described more fully hereinafter with reference to the accompanying drawings, in which preferred embodiments of the invention are shown. This invention may, however, be embodied in many different forms and should not be construed as limited to the embodiments set forth herein; rather, these embodiments are provided so that this disclosure will be thorough and complete, and will
15 fully convey the scope of the invention to those skilled in the art. Like numbers refer to like elements throughout.

 An APC ferrule **10**, such as an ST, SC, or FC ferrule, is provided that can be efficiently and repeatedly fabricated. As shown in Figures 1 and 2, the ferrule includes a ferrule body **12** extending lengthwise between the opposed front and rear faces **14**, **16**.
20 The ferrule is typically formed of a ceramic material, but can be formed of other materials, such as glass, if so desired. The ferrule body is generally cylindrical and defines a lengthwise extending bore **18** for receiving the end portion of an optical fiber such that the ferrule can be mounted thereupon. In this regard, the portion of the bore proximate the rear face of the ferrule body can taper radially outward in order to provide
25 a lead-in section **20** for funneling the optical fiber into the bore. Typically, the APC ferrule is designed to be mounted upon a single optical fiber, such as either a single-mode optical fiber or a multi-mode optical fiber.

 The ferrule body **12** also defines a longitudinal axis **22** extending lengthwise between the opposed front and rear faces **14**, **16** along the center line of the ferrule body.
30 In addition, the bore is also typically centered about the longitudinal axis. The ferrule can also include a chamfer **24** proximate the front face to facilitate the insertion and

alignment of a ferrule within a connector sleeve or the like and to reduce the size of the front face that must be ground and polished. Typically, the chamfer defines a 30° angle with respect to longitudinal axis. However, the chamfer can define other angles with respect to longitudinal axis, if so desired.

5 According to the present invention, the front face **14** of the ferrule body **12** is formed to include a plateau **26** and a hemispherical portion **28**. As depicted in Figures 1-3, the plateau defines a plane (designated **30** in Figure 3) that extends perpendicular to the longitudinal axis **22** of the ferrule body. In contrast, the hemispherical portion defines a spherical shape that is angled somewhat relative to the plane that extends perpendicular
10 to the longitudinal axis, thereby providing an angled front face that facilitates contact between the front face of the ferrule and another APC ferrule. Among other things, this physical contact reduces attenuation, typically to less than 0.3 dB with an average of about 0.1 dB. As shown, the plateau is preferably the forwardmost portion of the ferrule **10** with the hemispherical portion being continuous with the plateau, but generally
15 disposed somewhat rearward of the plateau. In addition, the hemispherical portion is formed such that the bore **18** defined by the ferrule body opens through the hemispherical portion. As such, the hemispherical portion typically extends across more than 50% of the front face of the ferrule body with the plateau extending across the remainder, i.e., less than 50%, of the front face of the ferrule body. In addition, the plateau is typically
20 disposed proximate a side surface of the ferrule body and, more particularly, proximate the chamfered portion **24** of the side surface of the ferrule.

 The hemispherical portion **28** of the front face **14** is preferably angled such that a plane **32** at a point coincident with the longitudinal axis **22**, i.e., coincident with the center line of the ferrule **10**, is disposed at an angle θ relative to the plane **30**, which is
25 perpendicular to the longitudinal axis and as depicted schematically in Figure 3. The offset angle is typically between 8° and 12° and, most typically, is 8°. As such, plane **32** is oftentimes called the 8° plane. By having an angled front face, the ferrule **10** of the present invention reduces disadvantageous reflections of the optical signals and facilitates the coupling of the optical signals between a pair of optical fibers upon which ferrules of
30 the present invention are mounted. For example, the ferrule typically reduces the optical reflections to -70 to -75 dB relative to the optical signals being transmitted.

As a result of its construction, the ferrule **10** also has a relatively small apex offset, that is, a relatively small offset between the apex **34** of the hemispherical surface and the bore **18** defined by the ferrule. In this regard, the apex is defined as the point on the hemispherical surface that protrudes the furthest outward from the ferrule body **12** relative to the plane **32**. As noted above, plane **32** is disposed at an angle θ relative to plane **32** and is coincident with the bore. By way of example, Figure 3 depicts a somewhat exaggerated apex offset **D** between the apex and the bore with the plane **32** depicted for purposes of explanation. Typically, the apex offset is less than 50 microns and, in some instances, is less than 10 microns with an average apex offset of approximately 30 microns. While an apex offset of 50 microns is generally sufficient to provide optical coupling between a pair of optical fibers upon which APC ferrules are mounted, APC ferrules that have a hemispherical portion **28** with a smaller radius of curvature may require an even smaller apex offset, such as 10 microns or less, in order to provide the desired optical coupling. In this regard, the hemispherical portion typically defines a radius of curvature between 5 millimeters and 12 millimeters. For a hemispherical portion having a radius of curvature of 5 millimeters, the ferrule of the present invention is particularly advantageous since the apex of the hemispherical surface can be repeatedly positioned to be within a relatively small distance, such as 10 microns or less, of the bore.

The ferrule **10** of the present invention can advantageously be fabricated in an efficient and repeatable manner by a method and an apparatus provided according to other aspects of the present invention. In this regard, the apparatus **40** for fabricating the ferrule includes a mounting fixture **42** for securely holding the ferrule such that the front face **14** of the ferrule is exposed. See Figure 4. Prior to the grinding process described below, the front face of the ferrule is generally planar and is perpendicular to the longitudinal axis **22** defined by the ferrule body **12**. As shown in Figure 5, the ferrule is also typically mounted in a ferrule holder **44** during the grinding process. As shown, the ferrule holder defines a well **46** that opens through one end for snugly receiving the rear end of the ferrule. Preferably, the well defined by the ferrule holder is sized such that a predetermined length of the ferrule (termed the "press length") extends outwardly beyond the ferrule holder. In one embodiment, the mounting fixture is a collet **43** in which the

ferrule holder and the ferrule are inserted. In particular, the collet of this embodiment includes a plurality of collet jaws 43 for engaging the side surface of the ferrule, as shown in Figure 4.

The apparatus 40 for fabricating the ferrule 10 also includes a grinder 48. As depicted schematically in Figure 6, the grinder includes a spindle 50 adapted for rotation about a spindle axis 52 and a grinding wheel 54 mounted upon the spindle for rotation therewith about the spindle axis. Typically, the grinding wheel includes an outer grinding surface 56 that includes grit of a predetermined size to facilitate grinding of the front face of the ferrule. In one embodiment, for example, the grinding surface may include diamond granules or grit having an average size of about 15 microns. In order to form the hemispherical portion 28 of the front face 14 of the ferrule as described below, the grinding surface of the grinding wheel is preferably arcuate and defines a predetermined radius of curvature. In order to form a hemispherical surface having a radius of curvature between 5 millimeters and 12 millimeters, the arcuate grinding surface of the grinding wheel also preferably defines a radius of between 5 millimeters and 12 millimeters since the radius of curvature of the arcuate grinding surface defines the corresponding radius of curvature of the resulting hemispherical portion of the front face of the ferrule.

The apparatus 40 for fabricating the ferrule 10 also preferably includes a plurality of adjustment stages 58 for adjusting the position of at least one of the mounting fixture 42 and the grinder 48 in respective planes relative to the other of the mounting fixture and the grinder. Typically, the mounting fixture is positioned in respective planes relative to the grinder by the plurality of adjustment stages. In this regard, the plurality of adjustment stages can adjust the position of the mounting fixture in at least two orthogonal directions, such as an upward/downward direction and a lateral direction. The position of the mounting fixture and, in turn, the ferrule, can be accurately aligned with respect to the grinding wheel 52.

In addition to rotating the spindle 50 and the grinding wheel 54 about the spindle axis 52, the grinder 48 is also adapted to rotate both the spindle and the grinding wheel about an offset axis 60 as depicted in Figure 6. As shown, the offset axis is perpendicular to the spindle axis and is coplanar with both the spindle axis and the longitudinal axis 22

defined by the ferrule body **12**. The grinder is adapted to rotate the spindle and the grinding wheel about the spindle axis at a faster rate, however, than the rate at which the grinder rotates both the spindle and the grinding wheel about the offset axis. For example, the grinder typically rotates the spindle and the grinding wheel about the spindle axis at a rate of approximately 10,000 rpm, while the grinder rotates the spindle and the grinding wheel about the offset axis at a rate of about 60 rpm. As a result of the simultaneous rotation about the spindle axis and the offset axis and the arcuate shape of the grinding surface, the grinder can impart the desired hemispherical shape to a portion **28** of the front face **14** of the ferrule **10**.

10 The apparatus **40** for fabricating the ferrule **10** also includes a translation device **62**, such as a translation stage, for advancing at least one of the grinder **48** and the mounting fixture **42** toward the other along a motion axis **64**. While either or both of the grinder and the mounting fixture can be moved toward the other along the motion axis, the grinder is typically carried by the translation stage that is controllably moved along a linear slide, while the mounting fixture generally fixes the ferrule in position following alignment of the ferrule with respect to the grinding wheel **54**. As such, the translation stage generally advances the grinder toward the ferrule along the motion axis defined by the linear slide at a predetermined feed rate. As shown schematically in Figure 6, the motion axis extends parallel to the longitudinal axis **22** defined by the ferrule body **12** and is coplanar with the spindle axis **52**, the offset axis **60** and the longitudinal axis.

20 During the advancement of the grinder **48** toward the ferrule **10**, the grinder rotates the spindle **50** and the grinding wheel **54** about both the spindle axis **52** and the offset axis **60**, albeit at different rates as described above. Once the grinding surface **56** of the grinding wheel engages the front face **14** of the ferrule, the simultaneous rotation of the grinding wheel about both the spindle axis and the offset axis imparts a hemispherical shape to a portion **28** of the front face due to the arcuate shape of the grinding surface.

Typically, the rates at which the grinder rotates the spindle and the grinding wheel about the spindle axis and the offset axis as well as the feed rate at which the translation device **62** advances the grinder toward the ferrule define the material removal rate, with increased rates of rotation and/or an increased feed rate correspondingly increasing the

material removal rate. While the grinder **48** can be advanced at different feed rates, the grinder of one embodiment is advanced at a feed rate of about 0.06 mm/sec.

As a result of the spindle axis being offset from the plane **30** perpendicular to the longitudinal axis **22** defined by the ferrule body **12** by the predetermined offset angle θ , typically between 8° and 12° , and the offset axis being correspondingly offset by the same predetermined angle from the longitudinal axis defined by the ferrule, the hemispherical surface is angled as described above.

The translation stage continues to advance the grinder **48** toward the ferrule **10** until a hemispherical portion **28** of the desired size has been formed. In this regard, since the ferrule extends beyond the ferrule holder **44** by a predetermined distance, i.e., the press length, and since the respective positions of the grinding wheel **54** and the mounting fixture **42** can be precisely determined with a laser micrometer or the like, the translation stage can controllably advance the grinder a predetermined distance toward the ferrule, with the predetermined distance being selected such that the hemispherical portion of the desired size is thereby formed. As shown in Figure 2, the hemispherical portion is preferably sized so as to encompass more than half of the front face **14** of the ferrule and to include that portion of the front face of the ferrule through which the bore **18** opens. However, advancement of the grinder toward the ferrule is preferably halted while the front face of the resulting ferrule still includes a plateau **26** so as to prevent unnecessary wear of the grinding wheel.

As a result of the fabrication technique of the present invention including the simultaneous rotation of the spindle **50** and the grinding wheel **54** about both the spindle axis **52** and the offset axis **60** and the concurrent advancement of the grinder **48** toward the ferrule **10** along the motion axis **64**, the resulting hemispherical portion **28** has an apex **34** that is either coincident with or spaced only slightly from the bore **18**, regardless of the depth to which the ferrule is ground. Thus, the fabrication method is repeatable such that the resulting ferrules are of a consistent quality.

According to the present invention, the plateau **26** is designed to accommodate any differences in the press length of the ferrule **10**, that is, the length of the ferrule that extends beyond the ferrule holder **44**. In this regard, if the ferrule is either slightly longer than normal or is not pressed as deeply as normal into the well **46** defined by the ferrule

holder, the grinder **48** will actually move more material resulting in a larger hemispherical portion **28** and a smaller plateau. In contrast, a slightly shorter ferrule or a ferrule that is pressed more deeply into the well defined by the ferrule holder will be ground less such that the plateau will be larger and the hemispherical portion will be smaller. In either instance, however, the apex of the hemispherical portion will still either be coincident with or only slightly offset from the bore **18** defined by the ferrule and the amount of any apex offset will be consistent irrespective of mount of material that is removed.

In addition, the fabrication method of the present invention is quite efficient and the resulting hemispherical surface **28** need only be slightly polished in order to complete the fabrication process. In this regard, the size of the grit carried by the grinding wheel **54** and the rate at which the grinding wheel is rotated about the spindle axis **52** generally defines the surface roughness. For a grinding wheel with diamond grit of 15 microns and rotating at 10,000 rpm, the hemispherical portion of the front face **14** of the ferrule **10** is generally quite smooth with a surface roughness of about 100 to 400 nanometers as measured peak to valley. In addition, the plateau generally need not be polished, thereby further conserving polishing consumables and reducing fabrication time. As such, the ferrule does not require extensive post-grinding operations and the resulting fabrication costs may therefore be reduced relative to conventional techniques for fabricating APC ferrules.

Many modifications and other embodiments of the invention will come to mind to one skilled in the art to which this invention pertains having the benefit of the teachings presented in the foregoing descriptions and the associated drawings. Therefore, it is to be understood that the invention is not to be limited to the specific embodiments disclosed and that modifications and other embodiments are intended to be included within the scope of the appended claims. Although specific terms are employed herein, they are used in a generic and descriptive sense only and not for purposes of limitation.